

## CIRCUIT AND METHOD FOR DEMODULATING A SERVO POSITION BURST

### Cross-reference to Related Applications

[1] This application is related to U.S. Patent Application Ser. Nos. \_\_\_\_\_  
5 (Atty. Docket No. 99-S-190 (1678-22-1)) entitled "DATA-STORAGE DISK HAVING  
FEW OR NO SPIN-UP WEDGES AND METHOD FOR WRITING SERVO WEDGES  
ONTO THE DISK," \_\_\_\_\_ (Atty. Docket No. 01-S-044 (1678-22-2)) entitled  
"CIRCUIT AND METHOD FOR DETECTING A SERVO WEDGE ON SPIN UP OF A  
DATA-STORAGE DISK", \_\_\_\_\_ (Atty. Docket No. 01-S-047 (1678-22-3)) entitled  
10 "CIRCUIT AND METHOD FOR DETECTING A SPIN-UP WEDGE AND A  
CORRESPONDING SERVO WEDGE ON SPIN UP OF A DATA-STORAGE DISK", \_\_\_\_\_  
\_\_\_\_\_ (Atty. Docket No. 01-S-023 (1678-39)) entitled "A DATA CODE AND  
METHOD FOR CODING DATA", \_\_\_\_\_ (Atty. Docket No. 01-S-045 (1678-48)) entitled  
"CIRCUIT AND METHOD FOR DETECTING THE PHASE OF A SERVO SIGNAL", \_\_\_\_\_  
15 \_\_\_\_\_ (Atty. Docket No. 01-S-054 (1678-49)) entitled "SERVO CIRCUIT  
HAVING A SYNCHRONOUS SERVO CHANNEL AND METHOD FOR  
SYNCHRONOUSLY RECOVERING SERVO DATA", which were filed on the same day  
as the present application and which are incorporated by reference.

### Field of the Invention

[2] The invention is related generally to electronic circuits, and more  
particularly to a circuit and method for demodulating a read-write-head position burst in  
a servo wedge without the need for over sampling or synchronization between the  
sample clock and the servo burst. Such a circuit and method often allows the position  
25 bursts to have a higher frequency, thus allowing the bursts to occupy less space on a  
disk. Furthermore, such a circuit and method often provide more accurate  
demodulation of the position burst — and thus often allow a more accurate positioning  
of the read-write head — because their accuracy is unaffected by disk jitter or other  
events that often degrade the synchronization between the sample clock and the servo  
30 signal.

## BACKGROUND OF THE INVENTION

[3] As software applications become larger and more data intensive, disk-drive manufacturers are increasing the data-storage capacities of data-storage disks by increasing the disks' data-storage densities (bits/inch). This increase in storage density typically increases the frequency of the read signal from the read-write head of the disk drive that incorporates such a disk.

[4] Unfortunately, as discussed in more detail below in conjunction with FIGS. 1 – 5, increasing the density of the servo data, and thus increasing the frequency of the servo signal, may cause a disk drive's head-position circuit to improperly position the read-write head over a selected data track. A servo circuit typically heavily over samples or uses fewer synchronized samples of the servo signal to calculate the amplitudes of read-write head position bursts that are stored on the disk. Using these burst amplitudes, the disk drive calculates a head-position error signal, which the head-position circuit uses to position the head over the selected data track. But if the frequency of the servo signal is too high, the servo circuit may be unable to generate enough samples for over sampling or maintain synchronization between the sample clock and the servo burst, and thus may calculate inaccurate values for the burst amplitudes. Consequently, these inaccurate values may cause the disk drive to calculate an erroneous value for the head-position error signal, and thus may cause the head-position circuit to improperly position the head over the selected data track.

[5] FIG. 1 is a plan view of a conventional disk drive 10, which includes a magnetic data-storage disk 12, a read-write head 14, an arm 16, and a voice-coil motor 18. The disk 12 is partitioned into a number — here eight — of disk sectors 20a-20h, and includes a number — typically in the tens or hundreds of thousands — of concentric data tracks 22a-22n. Readable-writable application data is stored in respective data sectors (not shown) within each track 22. Under the control of the disk drive's head-position circuit (not shown in FIG. 1), the motor 18 moves the arm 16 to center the head 14 over a selected track 22.

[6] Referring to FIG. 2, conventional data servo wedges 24 — only servo wedges 24a - 24c are shown for clarity — include servo data that allows the

head-position circuit (not shown in **FIG. 2**) of the disk drive **10** (**FIG. 1**) to accurately position the read-write head **14** (**FIG. 1**) during a data read or write operation. The servo wedges **24** are located within each track **22** at the beginning — the disk **12** spins counterclockwise in this example — of each disk sector **20**. Each servo wedge **24** includes respective servo data that identifies the location (track **22** and sector **20**) of the servo wedge. Thus, the head-position circuit uses this servo data to position the head **14** over the track **22** selected to be read from or written to. The manufacturer of the disk drive **10** typically writes the servo wedges **24** onto the disk **12** before shipping the disk drive to a customer; neither the disk drive nor the customer alters the servo wedges **24** thereafter. Servo wedges like the servo wedges **24** are further discussed below in conjunction with **FIG. 3** and in commonly owned U.S. Patent App. Ser. No. 09/783,801, filed February 14, 2001, entitled "VITERBI DETECTOR AND METHOD FOR RECOVERING A BINARY SEQUENCE FROM A READ SIGNAL," which is incorporated by reference.

**[7]** **FIG. 3** is a diagram of the servo wedge **24a** of **FIG. 2**, the other servo wedges **24** being similar. Write splices **30a** and **30b** respectively separate the servo wedge **24a** from adjacent data sectors (not shown). An optional servo address mark (SAM) **32** indicates to the head-position circuit (not shown in **FIG. 3**) that the read-write head **14** (**FIG. 1**) is at the beginning of the servo wedge **24a**. A servo preamble **34** allows the servo circuit (not shown in **FIG. 3**) of the disk drive **10** (**FIG. 1**) to synchronize the sample clock to the servo signal (**FIG. 5**), and a servo synchronization mark (SSM) **36** identifies the beginning of a head-location identifier **38**. Once the beginning of the identifier **38** is identified, a disk-drive controller (**FIG. 9**) can determine the beginnings of head-position bursts A – N by counting cycles of the sample clock. The preamble **34** and SSM **36** are discussed in commonly owned U.S. Patent application numbers \_\_\_\_\_ (Atty. Docket No. 99-S-190 (1678-22-1)) entitled "DATA-STORAGE DISK HAVING FEW OR NO SPIN-UP WEDGES AND METHOD FOR WRITING SERVO WEDGES ONTO THE DISK," \_\_\_\_\_ (Atty. Docket No. 01-S-044 (1678-22-2)) entitled "CIRCUIT AND METHOD FOR DETECTING A SERVO WEDGE ON SPIN UP OF A DATA-STORAGE DISK", \_\_\_\_\_ (Atty. Docket No. 01-S-047 (1678-22-

3)) entitled "CIRCUIT AND METHOD FOR DETECTING A SPIN-UP WEDGE AND A CORRESPONDING SERVO WEDGE ON SPIN UP OF A DATA-STORAGE DISK", \_\_\_\_\_

\_\_\_\_\_ (Atty. Docket No. 01-S-054 (1678-49)) entitled "SERVO CIRCUIT HAVING A SYNCHRONOUS SERVO CHANNEL AND METHOD FOR

5 SYNCHRONOUSLY RECOVERING SERVO DATA", which are incorporated by reference. The location identifier **38** allows the head-position circuit to coarsely determine and adjust the position of the head **14** with respect to the surface of the disk **12** (FIG. 1). More specifically, the location identifier **38** includes a sector identifier **40** and a track identifier **42**, which respectively identify the disk sector **20** and the data track **22** — here the sector **20a** and the track **22a** — that contain the servo wedge **24a**.

10 Because the head **14** may read the location identifier **38** even if the head is not centered over the track **24a**, the servo wedge **24a** also includes the head-position bursts A - N, which allow the head-position circuit to finely determine and adjust the position of the head **14** as discussed below in conjunction with FIGS. 4 and 5.

15 [8] FIG. 4 is a close-up view of a portion **48** of the disk **10** (FIG. 1), the portion **48** including four sections **50A – 50D** of head-position bursts A – D, respectively. More specifically, the portion **48** includes adjacent tracks  $22_n - 22_{n+7}$ , the illustrated portions of which include the servo wedges **24** (FIG. 3), burst sections **50A – 50D**, and write splices **30** and/or application data. Each of the bursts in sections **50A – 50D** is  
20 two tracks wide in a radial direction and is staggered with respect to the tracks **22** such that the boundaries **52** and **54** between adjacent bursts in the same section are aligned with the centers of respective tracks **22**. For example, the boundary  $52_{i+1}$  between adjacent bursts  $A_j$  and  $A_{j+1}$  and  $B_j$  and  $B_{j+1}$  is aligned with the center of the track  $22_{n+2}$ . Furthermore, the bursts in each section **50A – 50D** alternate between a logic 1  
25 (represented by an "X") value and a logic 0 (represented by a blank, i.e., the absence of an "X") value, and the values of the bursts in sections **50A** and **50C** are opposite to the values of the adjacent bursts in sections **50B** and **50D**, respectively. For example, bursts  $A_j$ ,  $A_{j+1}$ , and  $A_{j+2}$  in section A have alternating values 0, 1, 0, respectively, and adjacent bursts  $A_{j+1}$  and  $B_{j+1}$  have opposite values logic 1 and logic 0, respectively. In

one example, logic 1 represents a nonzero voltage level, and logic 0 represents a zero voltage level.

[9] In operation, the head-position circuit (not shown in FIG. 4) uses the relative magnitudes of diagonally adjacent bursts in sections 50A and 50B or in sections 50C and 50D to center the head 14 (FIG. 1) over a desired track. For example, assume that the head-position circuit is to center the head 14 over the track  $22_{n+2}$ . First using a conventional technique omitted here for clarity, the head-position circuit coarsely positions the head 14 over or near the track  $22_{n+2}$  and reads the track identifier 42 (FIG. 3) that the head 14 is over. If the read track identifier belongs to the track  $22_{n+2}$ , then the head-position circuit determines that the head 14 is close enough to the track  $22_{n+2}$  to proceed with the fine positioning of the head. Because the boundary  $52_{i+1}$  is aligned with the center of the track  $22_{n+2}$ , to center the head 14 the disk drive 10 (FIG. 1) reads and compares the magnitudes of the diagonally adjacent bursts  $A_{j+1}$  and  $B_j$  and calculates a position-error signal proportional to the difference between the magnitudes of  $A_{j+1}$  and  $B_j$ . The head-position circuit uses this error signal to move the head 14 toward, and ideally over, the center of the track  $22_{n+2}$ .

[10] More specifically, the disk drive 10 (FIG. 1) and the head-position circuit (not shown in FIG. 4) operate according to Table I to center the head 14 (FIG. 1) over the track  $22_{n+2}$ , where Mag A equals the read-voltage level, *i.e.*, magnitude, of  $A_{j+1}$ , and Mag B equals the read-voltage level, *i.e.*, magnitude, of  $B_j$  ( $A_j$  and  $B_{j+1}$ , which are logic 0, have zero voltage levels in this example):

Table I

First Scenario	Mag A > Mag B	To center the head over track <b>22<sub>n+2</sub></b> if the head <b>14</b> is not centered over the track <b>22<sub>n+2</sub></b> and is closer to the track <b>22<sub>n+3</sub></b> , the head-position circuit needs to moves the head <b>14</b> toward/to the center of the track <b>22<sub>n+2</sub></b> in a direction toward the center (bottom of <b>FIG. 4</b> ) of the disk <b>10</b> .
Second Scenario	Mag A = Mag B	The head <b>14</b> is centered over the track <b>22<sub>n+2</sub></b> . Therefore, the head-position circuit does not need to move the head <b>14</b> for track <b>22<sub>n+2</sub></b> centering..
Third Scenario	Mag A < Mag B	The head <b>14</b> is not centered over the track <b>22<sub>n+2</sub></b> , and is closer to the track <b>22<sub>n+1</sub></b> . Therefore, the head-position circuit moves the head <b>14</b> toward/to the center of the track <b>22<sub>n+2</sub></b> in a direction toward the center of the disk <b>10</b> .

[11] To illustrate the first scenario, assume that after coarse positioning, the head **14** is over the track **22<sub>n+3</sub>** at a position R, which is a radial distance +Dr from the center M of the track **22<sub>n+2</sub>** — the center M is aligned with the boundary **52<sub>i+1</sub>**. When the disk **10** (**FIG. 1**) rotates such that the head **14** is aligned with the burst section **50A**, the burst **A<sub>j+1</sub>** is directly beneath the head such that the servo-signal voltage level, Mag A, has a maximum value. Conversely, when the disk **10** rotates such that the head **14** is aligned with the burst section **50B**, the head is radially spaced +Dr from the boundary **52<sub>i+1</sub>**, and thus from the burst **B<sub>j</sub>**, such that the servo-signal voltage level, Mag B, has a nonmaximum value that is less than Mag A. Because Mag A > Mag B, the disk drive **10** “knows” the direction of the head-position error, *i.e.*, that the head **14** is closer to the track **22<sub>n+3</sub>** than to the track **22<sub>n+1</sub>**. Furthermore, |Mag A – Mag B| is proportional



to the distance  $D_r$  between the head **14** and the center of the track  $22_{n+2}$ . Therefore, Mag A and Mag B together provide the disk drive **10** with the magnitude and direction of the head-position error, and the disk drive uses this vector to generate a position-error signal. In response to the position-error signal, the head-position circuit (not shown in **FIG. 4**) causes the motor **18** (**FIG. 1**) to reduce the head-position error by moving the head **14** from the position R toward/to the center M of the track  $22_{n+2}$ .

[12] To illustrate the second scenario, assume that after coarse positioning, the head **14** is over the center M of the track  $22_{n+2}$ . When the head **14** is over the burst sections **50A** and **50B**, it is aligned with the boundary  $52_{i+1}$ . Because the boundary  $52_{i+1}$  is equidistant from the bursts  $A_{j+1}$  and  $B_j$  in a radial direction,  $\text{Mag A} = \text{Mag B}$ . Because  $\text{Mag A} = \text{Mag B}$ , the disk drive **10** "knows" that the head **14** is centered over the track  $22_{n+2}$ , and thus "knows" that no position correction is necessary. This follows from  $|\text{Mag A} - \text{Mag B}| = 0$ , which indicates that the error distance is zero.

[13] To illustrate the third scenario, assume that after coarse positioning, the head **14** is over the track  $22_{n+1}$  at a position Q, which is a radial distance  $-D_q$  from the center M of the track  $22_{n+2}$  — "-" indicates that  $D_q$  and  $D_r$  are in opposite directions from M. Therefore, because  $\text{Mag B} > \text{Mag A}$ , the disk drive **10** "knows" that the head **14** is closer to the track  $22_{n+1}$  than to the track  $22_{n+3}$ , and thus generates a corresponding position-error signal. In response to this position-error signal, the head-position circuit that causes the motor **18** to move the head **14** from Q toward/to the center M of the track  $22_{n+2}$ .

[14] Although the servo-wedge portions (to the left of the bursts **50A** – **50D**) of the tracks **22** are shown as having the same widths as the corresponding data-sector portions (to the right of the bursts **50A** – **50D**) portions, these portions may have different widths. Where the widths are different, the boundaries **52** and **54** are aligned with the centers of the data-sector portions to accurately read the application data.

[15] **FIG. 5** is a plot of a sinusoidal servo signal that the head **14** (**FIG. 1**) generates while reading a head-position burst, and a sample clock that is not synchronized to the burst sinusoid.

[16] According to one conventional technique, the servo circuit (not shown in FIG. 5) synchronizes the sample clock to the servo signal as the head 14 reads the preamble 34 (FIG. 3). Typically, this preamble servo signal (not shown) is a sinusoid similar or identical to the burst sinusoid, and the servo circuit aligns the edges of the sample clock to the peaks and zero crossings of the preamble sinusoid. For example, the servo circuit may align the rising edges of the servo clock with the peaks and the falling edges with the zero crossings. Unfortunately, by the time that the head 14 is over the position-burst sections 50A – 50D (FIG. 4), phenomena such as noise and disk jitter may cause the edges of the sample clock to become offset from the peaks and zero crossings of the burst sinusoid. For example the rising and falling edges of the sample clock may respectively lead the peaks and zero crossings of the burst sinusoid by a nonzero angle  $\alpha$ , where it is desired that  $\alpha$  equal zero.

[17] Unfortunately, the lack of synchronization between the sample clock and the burst sinusoid may cause the head-position circuit (not shown in FIG. 5) to improperly position the head 14 over the selected track 22 (FIG. 4) during the fine positioning of the head. Typically, the peak voltage level Y of the burst sinusoid is the magnitude (e.g., Mag A or Mag B of FIG. 4) of the position burst. In FIG. 4 for example,  $|Y| > 0$  represents a logic 1 (represented by an "X") and  $Y = 0$  (DC signal) represents a logic 0 (represented by the absence of "X"). Furthermore, the accuracy of the algorithm that the disk drive 10 (FIG. 1) uses to demodulate, i.e., calculate the magnitudes of, the position bursts is often proportional to the level of synchronization between the sample clock and the burst sinusoid. For example, assuming perfect synchronization, the samples 60 taken at the rising edges of the sample clock are of the burst-sinusoid peaks, and thus equal Y. Therefore, a simple algorithm averages a number of the samples 60 to filter out noise and calculates the burst magnitude equal to this average. But if the clock and burst sinusoid are imperfectly aligned as shown, then, ignoring noise and jitter, this algorithm yields an incorrect burst magnitude  $Y \cos \alpha$  instead of the correct burst magnitude Y. This incorrect burst magnitude may cause the disk drive 10 to calculate an inaccurate position-error signal, which may cause the motor 18 (FIG. 1) to move the head 14 to an undesired position.



[18] Still referring to **FIG. 5**, according to another conventional technique, one can overcome the above-described lack of synchronization by heavily oversampling the burst sinusoid. To oversample, one increases the frequency of the sample clock with respect to the burst sinusoid. But because there are often constraints on the speed of the sample clock, one typically reduces the frequency of the burst sinusoid by lengthening the bursts **50A – 50D** (**FIG. 4**). To obtain accurate estimation of the burst amplitude **Y**, it is generally accepted that the sample clock must generate at least ten samples per cycle of the burst sinusoid, and thus must have a frequency at least five times that of the burst sinusoid. Comparitively, for the above-described synchronous technique, the sample clock generates four samples **60** and **62** per cycle and has a frequency that is twice that of the burst sinusoid as shown in **FIG. 5**.

[19] Unfortunately, although heavily oversampling allows one to calculate the burst amplitude **Y** with an unsynchronized sampling clock, it typically requires more disk space due to the above-described lengthening of the position bursts **50A – 50D** (**FIG. 4**).

#### SUMMARY OF THE INVENTION

[20] In accordance with an embodiment of the invention, a circuit receives fewer than ten samples per cycle of a position burst and calculates the burst magnitude from the samples such that the accuracy of the burst magnitude is independent of the timing of the samples with respect to the burst.

[21] By using an algorithm that does not require heavy over sampling — for purposes of this application, heavy over sampling is a sampling rate more than four samples per cycle — and that is independent of the level of synchronization between the sample clock and the position bursts, such a circuit often allows shorter position bursts than a heavy-over-sampling circuit allows and calculates the burst magnitudes and the head-position-error signal more accurately than a circuit that uses a timing-dependent algorithm.

### BRIEF DESCRIPTION OF THE DRAWINGS

[22] FIG. 1 is a plan view of a conventional disk drive.

[23] FIG. 2 is a close-up view of some tracks and servo wedges on the disk  
5 of FIG. 1.

[24] FIG. 3 is a diagram of a servo wedge of FIG. 2.

[25] FIG. 4 is a close-up view of some tracks and position bursts on the disk  
of FIG. 1.

10 [26] FIG. 5 is a plot of a conventional burst sinusoid and a conventional sample  
clock that is not synchronized to the burst sinusoid.

[27] FIG. 6 is a block diagram of a position-burst demodulator according to an  
embodiment of the invention.

[28] FIG. 7 is a phase diagram used to explain how the demodulator of FIG. 6  
calculates the magnitude of a position burst according to an embodiment of the  
15 invention.

[29] FIG. 8 is a block diagram of a servo circuit that incorporates the  
position-burst demodulator of FIG. 6 according to an embodiment of the invention.

[30] FIG. 9 is a block diagram of a disk-drive system that incorporates the  
servo circuit of FIG. 8 according to an embodiment of the invention.  
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### DESCRIPTION OF THE PREFERRED EMBODIMENTS

[31] FIG. 6 is a block diagram of a position-burst demodulator 70 according to  
an embodiment of the invention. As discussed below in conjunction with FIG. 7, the  
circuit uses a variation of a known trigonometric identity to calculate the magnitude of a  
25 position burst (FIGS. 4 and 5) independently of the synchronization, or lack thereof,  
between the sample clock (FIG. 5) and the position burst. In the embodiment discussed  
in conjunction with FIG. 6, the demodulator 70 is part of a servo circuit (FIG. 8) and  
provides a head-position-error signal to a head-position circuit (FIG. 9). Alternatively,  
the demodulator 70 may be part of the head-position circuit.

**[32]** FIG. 7 is a phase diagram of a positive half period of the burst sinusoid of FIG. 5, and illustrates how the position-burst demodulator 70 of FIG. 6 calculates a synchronization-independent value for the magnitude Y of the burst sinusoid. Specifically, samples 90 and 92 are 90° apart. Therefore, one can calculate the amplitude Y according to the following equations, which follow from the well-known trigonometric identity  $\sin^2\beta + \cos^2\beta = 1$ :

$$(1) \quad (Y\sin\beta)^2 + (Y\cos\beta)^2 = Y^2\sin^2\beta + Y^2\cos^2\beta = Y^2(\sin^2\beta + \cos^2\beta) = Y^2$$

$$(2) \quad \text{Sample } 90 = Y\sin\beta_2$$

$$(3) \quad \text{Sample } 92 = Y\cos\beta_2$$

$$(4) \quad Y^2 = (\text{sample } 90)^2 + (\text{sample } 92)^2$$

$$(5) \quad Y = \sqrt{(\text{sample } 90)^2 + (\text{sample } 92)^2}$$

Further details of this identity are discussed in commonly owned U.S. Patent App. Ser. No. 09/503,949, filed February 14, 2000, entitled "A CIRCUIT AND METHOD FOR CONTROLLING THE GAIN OF AN AMPLIFIER BASED ON THE SUM OF SAMPLES OF THE AMPLIFIED SIGNAL", and U.S. Patent App. Ser. No. 09/503,399, filed February 14, 2000, entitled "A CIRCUIT AND METHOD FOR CONTROLLING THE GAIN OF AN AMPLIFIER", which are incorporated by reference.

**[33]** Referring again to FIG. 6, in one embodiment the demodulator 70 improves upon the above-described trigonometric identity by effectively averaging the samples of the burst sinusoid of FIGS. 5 and 7 to filter out noise. For example purposes, the operation of the demodulator 70 is described where the head-position circuit (FIG. 9) is attempting to center the head 14 (FIGS. 1 and 9) over the track  $22_{n+2}$  (FIG. 4), it being understood that the operation of the demodulator 70 is similar when the head-position circuit attempts to center the head over another track.

**[34]** More specifically, referring to FIGS. 4 - 6, an adder 72a sums the magnitudes of a number — for example eight — of even samples 60 of the position burst  $A_{j+1}$  to generate a sum E, and an adder 72b sums the magnitudes of the same number of odd samples 62 of the same position burst to generate a sum O. In one

embodiment, the adders **72a** and **72b** respectively generate the sums E and O by summing the negative of every other sample. For example, the even sample **60a** is positive, but the next even sample **60b** is negative. Therefore, the adder **72a** sums the samples **60a** and **60c**, which are positive values, with the negatives of the samples **60b** and **60d**, these negatives also being positive values (the negative of a negative is a positive). Likewise, the adder **72b** sums the samples **62a** and **62c** with the negatives of the samples **62b** and **62d**. Although one could generate E equal to a single sample **60** and O equal to a single sample **62**, summing multiple samples **60** and **62** to respectively generate E and O averages out noise that may contaminate the burst sinusoid.

[35] The functions of the adders **72a** and **72b** is represented by the following equations:

$$(6) \quad E = (\text{sample } 60a - \text{sample } 60b) + (\text{sample } 60c - \text{sample } 60d) \dots$$

$$(7) \quad O = (\text{sample } 62a - \text{sample } 62b) + (\text{sample } 62c - \text{sample } 62d) \dots$$

[36] Next, multipliers **74a** and **74b** respectively square E and O and a summer **76** sums  $E^2$  and  $O^2$  according to equation (4), where E effectively corresponds to "sample **90**" and O effectively corresponds to "sample **92**".

[37] Then, a root circuit **78** takes the square root of  $E^2 + O^2$  to generate the magnitude Mag A of the burst  $A_{j+1}$ , and stores Mag A in a first memory **80a**.

[38] Next, the demodulator **70** calculates the magnitude Mag B of the burst  $B_j$  in a similar manner and stores Mag B in a second memory **80b**.

[39] Then, a subtractor **82** calculates the head-position-error signal equal to  $\text{Mag B} - \text{Mag A}$ . The polarity (+ or -) of the signal indicates the direction of the error, and the value  $|\text{Mag B} - \text{Mag A}|$  indicates the magnitude of the error. Using the error signal, the head-position circuit (**FIG. 9**) finely positions the head **14** as discussed above in conjunction with **FIG. 4**. In other embodiments, however, the subtractor **82** may calculate the error signal equal to  $\text{Mag A} - \text{Mag B}$ , or the demodulator **70** or head-position circuit may further process the error signal before using it to finely position the head **14**.

[40] Although the demodulator **70** is described as including respective circuit blocks **72a** – **80b**, in other embodiments the demodulator may include a processor or logic circuit programmed to implement the above-described algorithm. Furthermore, the demodulator **70** may use other algorithms to calculate  $E^2$ ,  $O^2$ , and MAG A and MAG B.

5 For example, the circuit **70** can square an even sample **60** to generate  $E^2$ , square the next odd sample **62** to generate  $O^2$ , take the square root of  $E^2 + O^2$ , and sum the resulting square roots of  $E^2 + O^2$  over a number of samples **60** and **62** to obtain MAG A or MAG B. Other algorithms are contemplated but are omitted for brevity.

[41] FIG. 8 is block diagram of a synchronous servo circuit **100**, which includes  
10 the position-burst demodulator **70** of FIG. 6 according to an embodiment of the invention. The circuit **100** includes a gain and filter circuit **102**, which adjusts the gain and filters the servo signal from the read head **14**. An analog-to-digital converter (ADC) **104** receives the sample clock (FIG. 5) on a control bus **106** and generates digital samples, such as the samples **60** and **62** (FIG. 5), of the analog servo signal from the circuit **102**. A finite-impulse-response (FIR) filter **108** equalizes the samples from the ADC **104**, and timing and gain recovery loops **110** effectively synchronize the sample clock to the servo signal and maintain the gain of the circuit **100** at a desired level. In one embodiment, the circuit **102** and FIR filter **108** equalize the servo signal to a PR4 target, although they may equalize the servo signal to another target such as EPR4. A Viterbi detector **112** recovers servo data such as the location identifier **38**  
15 (FIG. 3) from the servo-signal samples, and a sync-mark detector **114** recovers the servo sync mark **36** (FIG. 5) from the servo signal. If the servo data is encoded, a decoder **116** decodes the recovered servo data and sync mark from the Viterbi and sync mark detectors **112** and **114**, respectively. The position-burst demodulator **70**  
20 receives the even and odd samples **60** and **62** (FIG. 5) from the FIR **108** and generates the head-position-error signal, and a processor **118** controls the components of the servo circuit **100** via the control bus **106**. A servo-data interface **120** interfaces the decoder **116**, processor **118**, and demodulator **70** to a disk-drive controller (FIG. 9).

[42] Because the demodulator **70** implements a timing-independent algorithm  
30 as discussed above, it can calculate the position-error signal without introducing



additional latency into the algorithm. Specifically, the timing-recovery portion of the loops **110** synchronizes the sample clock to the servo signal by shifting the values of the samples, not by shifting the phase of the sample clock. Therefore, if the demodulator **70** required synchronized samples, it would need to receive them from a point after the timing-loop portion of the loops **110**, which would introduce significant latency into the burst-demodulation calculation. But because the burst-demodulation algorithm is timing independent, the demodulator **70** can receive the potentially unsynchronized burst samples from the FIR **108**, and thus calculate the position-error signal without the latency of the loops **110**.

**[43]** Still referring to **FIG. 8**, the circuit **102**, ADC **104**, FIR **108**, loops **110**, Viterbi detector **112**, decoder **116**, processor **118** and operation of the servo circuit **100** are further discussed in commonly owned patent applications \_\_\_\_\_ (Atty. Docket No. 99-S-190 (1678-22-1)) entitled "DATA-STORAGE DISK HAVING FEW OR NO SPIN-UP WEDGES AND METHOD FOR WRITING SERVO WEDGES ONTO THE DISK," \_\_\_\_\_ (Atty. Docket No. 01-S-044 (1678-22-2)) entitled "CIRCUIT AND METHOD FOR DETECTING A SERVO WEDGE ON SPIN UP OF A DATA-STORAGE DISK", \_\_\_\_\_ (Atty. Docket No. 01-S-047 (1678-22-3)) entitled "CIRCUIT AND METHOD FOR DETECTING A SPIN-UP WEDGE AND A CORRESPONDING SERVO WEDGE ON SPIN UP OF A DATA-STORAGE DISK", \_\_\_\_\_ (Atty. Docket No. 01-S-054 (1678-49)) entitled "SERVO CIRCUIT HAVING A SYNCHRONOUS SERVO CHANNEL AND METHOD FOR SYNCHRONOUSLY RECOVERING SERVO DATA". The timing-recovery loop of the loops **110** is further discussed in commonly owned U.S. Patent App. Ser. No. 09/387,146, filed August 31, 1999, entitled "DIGITAL TIMING RECOVERY USING BAUD RATE SAMPLING", and the gain-recovery loop of the loops **110** and the Viterbi detector **112** are also discussed in commonly owned Patent App. Ser. No. 09/783,801, (Atty. Docket No. 99-S-185 (1678-21)), filed February 14, 2001, entitled "VITERBI DETECTOR AND METHOD FOR RECOVERING A BINARY SEQUENCE FROM A READ SIGNAL," all of which are incorporated by reference. The sync mark detector **114** is further discussed in commonly owned patent application \_\_\_\_\_ (Atty. Docket No. 01-S-045 (1678-48)) entitled "CIRCUIT AND METHOD

FOR DETECTING THE PHASE OF A SERVO SIGNAL", and the decoder **116** may be constructed to decode servo data that is encoded according to the scheme discussed in commonly owned U.S. Patent App. Ser. Nos. 09/783,801, (Atty. Docket 99-S-185 (1678-21)), filed February 14, 2001, entitled "VITERBI DETECTOR AND METHOD FOR RECOVERING A BINARY SEQUENCE FROM A READ SIGNAL", or the scheme discussed in \_\_\_\_\_ (Atty. Docket No. 01-S-023 (1678-39)) entitled "A DATA CODE AND METHOD FOR CODING DATA", which are incorporated by reference.

**[44]** **FIG. 9** is a block diagram of a disk-drive system **200** that incorporates the servo circuit **100** of **FIG. 8** according to an embodiment of the invention, where like numbers reference components common to **FIGS. 1** and **9**. The disk-drive system **200** includes a disk drive **202**, which incorporates the servo circuit **30** of **FIG. 8**. The disk drive **202** includes the read-write head **14**, a write channel **206** for generating and driving the head **14** with a write signal, and a write controller **208** for interfacing the write data to the write channel **206**. The disk drive **202** also includes a read channel **210** for receiving servo and application-data read signals from the head **32** and for recovering data from these read signals, and includes a read controller **212** for organizing the read data. Together, the write and read controllers **208** and **212** compose a disk-drive controller **213**. The read channel **210** includes the servo circuit **30**, which receives the servo signal from the head **14**, recovers the servo data from the servo signal, and provides the recovered servo data to a head-position circuit **214**. The disk drive **202** further includes a storage medium such as one or more disks **215**, each of which may contain data on one or both sides and which may be magnetic, optical, or another type of storage disk. For example, the disks **215** may be similar to the disk **12** of **FIG. 1**. The head **14** writes/reads the data stored on the disk **12**, and is connected to the movable support arm **16**. As discussed above in conjunction with **FIGS. 6-7**, the servo circuit **100** calculates the position-error signal, and, in response to the error signal, the head-position circuit **214** provides a control signal to the voice-coil motor (VCM) **18**, which positionally maintains/radially moves the arm **16** so as to positionally maintain/radially move the head **14** over the desired data tracks on the disks **215**. A

spindle motor (SPM) **220** and a SPM control circuit **222** respectively rotates the disks **215** and maintains them at the proper rotational speed.

**[45]** The disk-drive system **200** also includes write and read interface adapters **224** and **226** for respectively interfacing the disk-drive controller **213** to a system bus **228**, which is specific to the system used. Typical system busses include ISA, PCI, S-Bus, Nu-Bus, etc. The system **200** typically has other devices, such as a random access memory (RAM) **230** and a central processing unit (CPU) **232** coupled to the bus **228**.

**[46]** As discussed above, although the burst demodulator **70** (**FIG. 6**) is described as being part of the servo circuit **100**, it may be part of the head-position circuit **214** instead.

**[47]** From the foregoing it will be appreciated that, although specific embodiments of the invention have been described herein for purposes of illustration, various modifications may be made without deviating from the spirit and scope of the invention.